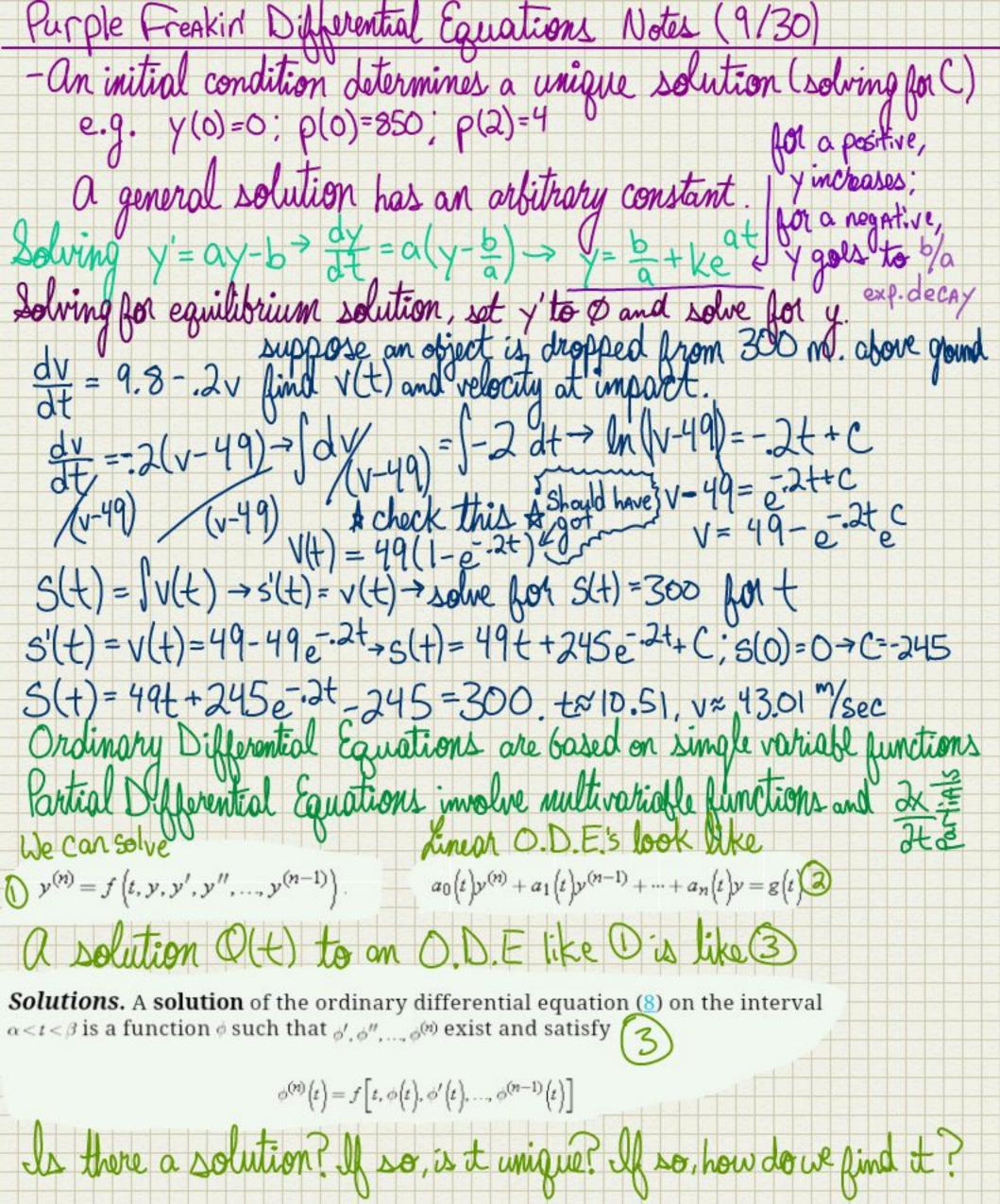
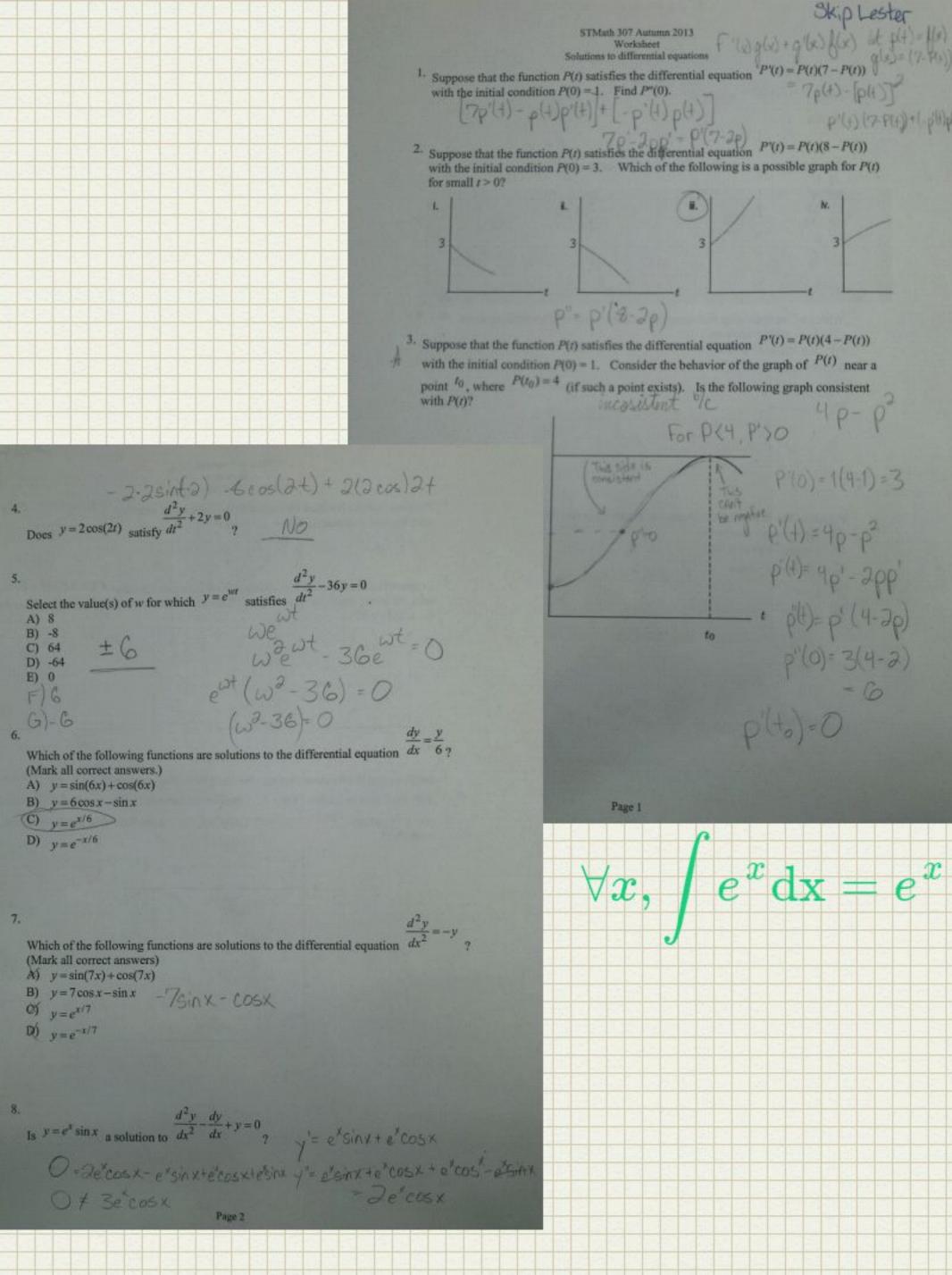
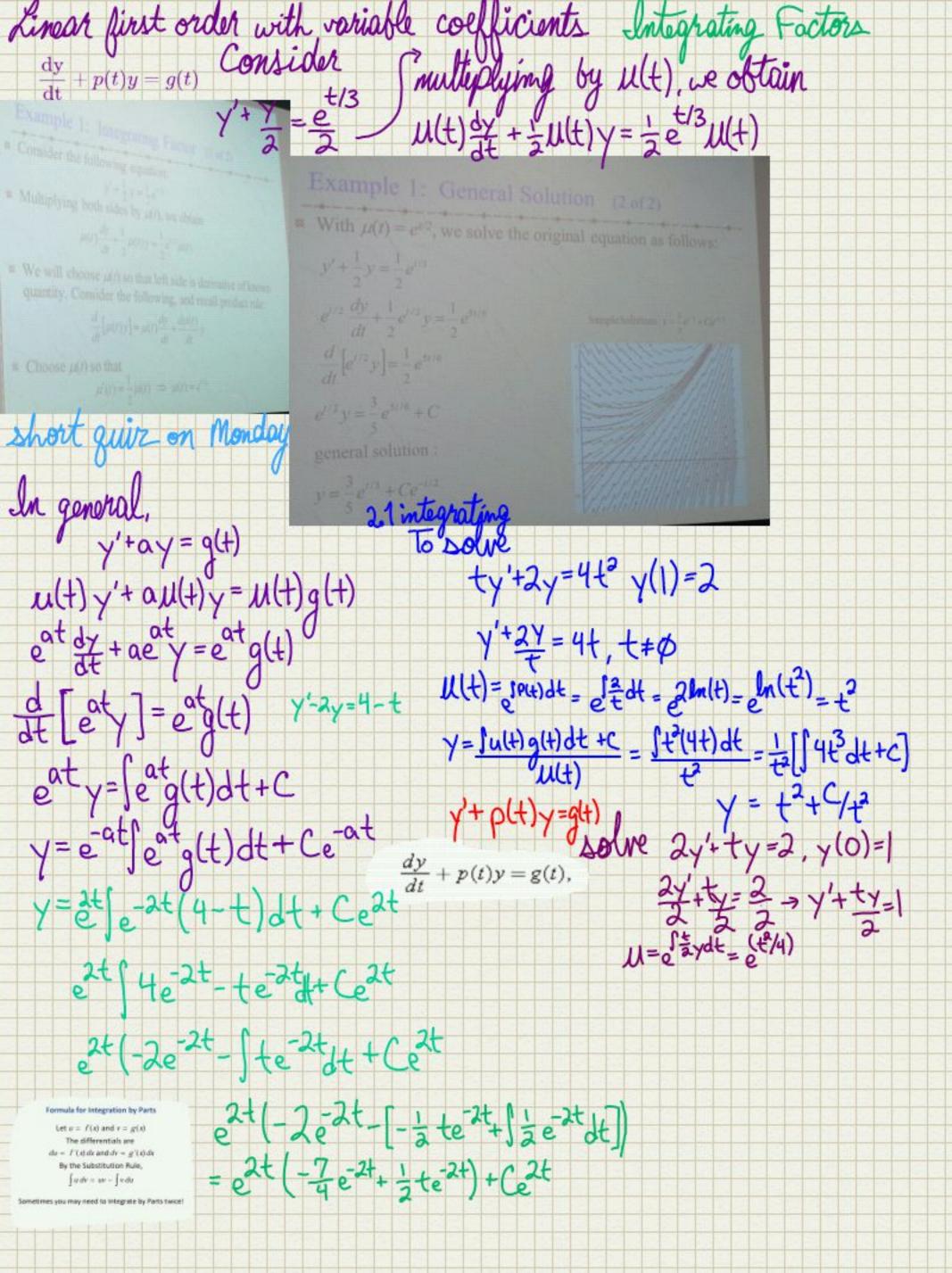
DFQ-STMATH 3077 - equations involving a function and its derivatives -deals with notes of change - mathematical model - simplified In general, for y'= ay-b, find eq. soln by setting y'=0

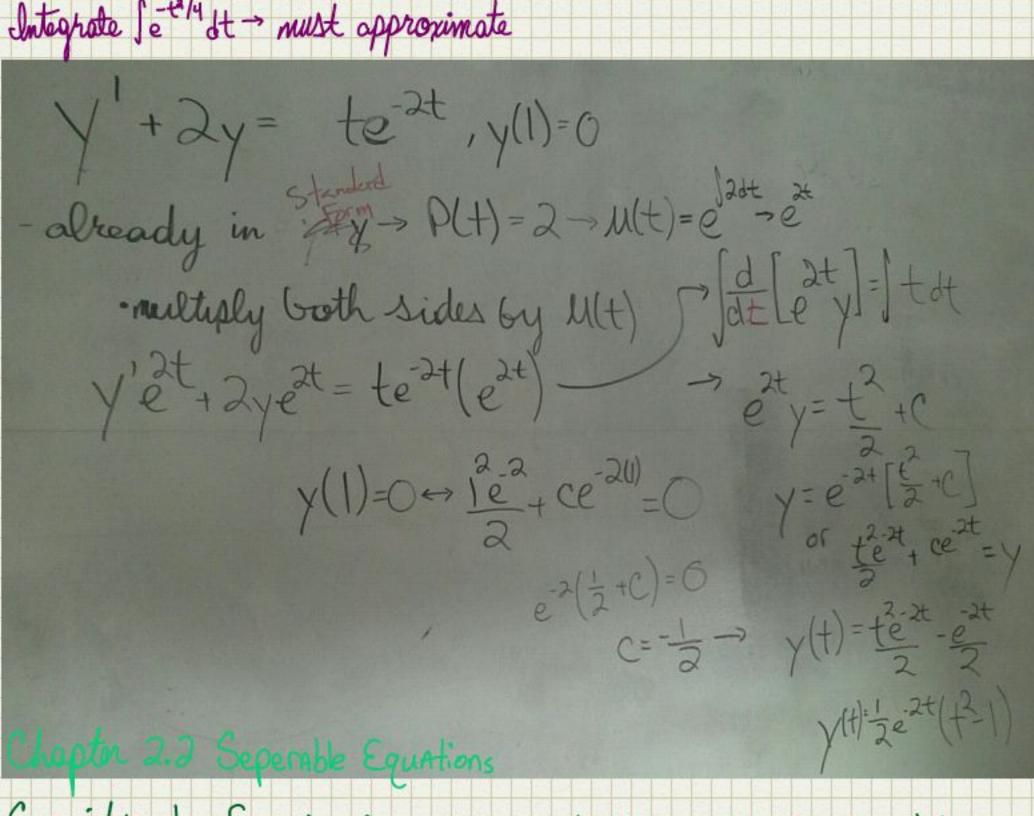
y(t)=b - can have several eq. solutions - identify independent +dependent variables -assign them rames Monday 30 Sep 13. Dolo Notes 9/30 We found the general solution p'= .5p -450 dP = .5(ρ-900) => dP/dt = .5 => [= 900] .5dt => lnlp-900|=.5t+C Prove that P is a solution. |P-900| = (.5t+C) = e = ke + p = 900 + ke + st |P-900| = (.5t+C) = e = ke + p = 900 + ke + st |P-900| = (.5t+C) = e = ke + st |P-900| = (.5t+C) = e = ke + st $\frac{dP}{dt} = \frac{k \cdot (t/2)}{2} \rightarrow \text{plug in } \frac{k}{2}e^{t/2} = \frac{5p-450}{2}$.5 (900 + ke*)-450 = Ke.5t 1



1.1 a pond initially contains 1,000,000 gallons of water and an unknown amount of an undesirable chemical. Water containing 0.04 gram of this chemical per gallon flows into the pond at a nate of 200 gal/hour. The mixture flows out at the same rate, so the amount of water in the pond remains constant. assume the chemical is uniformly distributed in the pond. Write a Differential Equation for the amount q (in grams) of chemical in the pond at any time t(in hours). de = 8 - 200 g 211) How many grams will be left after a very long time? The = (0.04)(200) - 200 9 - set to zero 5.00° (2 9 = 8 (5,000) 9 = 40,000 grams after large T 29a) a drug is being administered intravenously to a hospital patient. Fluid containing k=7 mg/cm3 of the drug enters the patients bloodstream at a rate of r= 50 cm3/nour. The drug is absorbed by body tissue or otherwise leaves the bloodstream at a rate proportional to the amount present with a rate constant of p=0.10 (hr"). Write a differential equation for the amount of drug present in the bloodstream at any time t. dq = K·r-pq > dq = (7 mg/cm3)(50 cm/hr) - (0.1 /hr)(q(t)) How much of the drug is present after a long time?







Consider $\frac{dy}{dx} = f(x,y)$; We can re-write this as $M(x,y) + N(x,y) \frac{dy}{dx} = 0$ Then M(x)dx + N(y)dy = 0 — can result in implicit

separable can be linear or non-linear relation of x and y. $\frac{dy}{dx} = 0$ $\frac{dy}{d$

2.2 Separable Equations

In <u>Section 1.2</u> and <u>Section 2.1</u> we used a process of direct integration to solve first order linear equations of the form

$$\frac{dy}{dt} = ay + b, (1)$$

where a and b are constants. We will now show that this process is actually applicable to a much larger class of equations.

We will use x, rather than t, to denote the independent variable in this section for two reasons. In the first place, different letters are frequently used for the variables in a differential equation, and you should not become too accustomed to using a single pair. In particular, x often occurs as the independent variable. Further, we want to reserve t for another purpose later in the section.

The general first order equation is

$$\frac{dy}{dx} = f(x, y). \tag{2}$$

Linear equations were considered in the preceding section, but if Eq. (2) is nonlinear, then there is no universally applicable method for solving the equation. Here, we consider a subclass of first order equations that can be solved by direct integration.

To identify this class of equations, we first rewrite Eq. (2) in the form

$$M(x, y) + N(x, y)\frac{dy}{dx} = 0. \qquad (3)$$

It is always possible to do this by setting M(x,y) = -f(x,y) and N(x,y) = 1, but there may be other ways as well. If it happens that M is a function of x only and N is a function of y only, then Eq. (3) becomes

$$M(x) + N(y)\frac{dy}{dx} = 0. (4)$$

Such an equation is said to be **separable**, because if it is written in the differential form

$$M(x)dx + N(y)dy = 0, (5)$$

then, if you wish, terms involving each variable may be placed on opposite sides of the equation. The differential form (5) is also more symmetric and tends to suppress the distinction between independent and dependent variables.

A separable equation can be solved by integrating the functions M and N. We illustrate the process by an example and then discuss it in general for Eq. (4).



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7.3 Separable Equations

Some differential equations can be solved explicitly. A **separable equation** is a first order differential equation in which the expression for $\frac{dy}{dx}$ can be factored as a function of x multiplied by a function of y.

$$\frac{dy}{dx} = g(x) f(y)$$

If
$$f(y) \neq 0$$
, we can write $\frac{dy}{dx} = \frac{g(x)}{h(y)}$, $h(y) = \frac{1}{f(y)}$.

Now we write it with x on one side and y on the other

$$h(y) dy = g(x) dx$$
...so we can integrate both sides! $\int h(y) dy = \int g(x) dx$

Sometime we can even solve for y in terms of x:

Differentiating implicitly on the left hand side and explicitly on the right,

$$\frac{d}{dx}\left(\int h(y)\,dy\right) = \frac{d}{dx}\left(\int g(x)\,dx\right) : \frac{d}{dy}\left(\int h(y)\,dy\right)\frac{dy}{dx} = g(x)$$

$$\therefore h(y)\frac{dy}{dx} = g(x)$$

Mixing

At time t=0 a tank contains Q_0 lb of salt dissolved in 100 gal of water; see Figure 2.3.1. Assume that water containing $\frac{1}{4}$ lb of salt/gal is entering the tank at a rate of r gal/min and that the well-stirred mixture is draining from the tank at the same rate. Set up the initial value problem that describes this flow process. Find the amount of salt Q(t) in the tank at any time, and also find the limiting amount Q_L that is present after a very long time. If r=3 and $Q_0=2Q_L$, find the time T after which the salt level is within 2% of Q_L . Also find the flow rate that is required if the value of T is not to exceed 45 min.

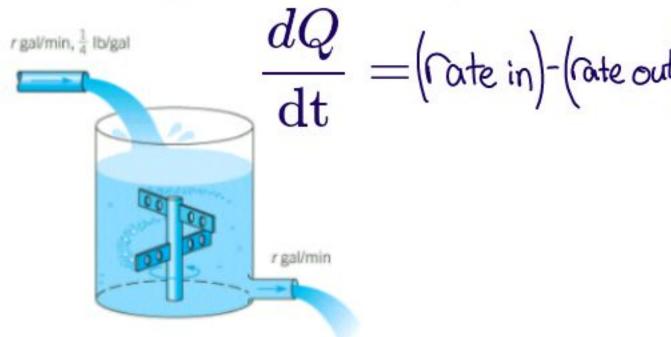


FIGURE 2.3.1 The water tank in Example 1.

We assume that salt is neither created nor destroyed in the tank. Therefore, variations in the amount of salt are due solely to the flows in and out of the tank. More precisely, the rate of change of salt in the tank, dQ / dt, is equal to the rate at which salt is flowing in minus the rate at which it is flowing out. In symbols,

$$\frac{dQ}{dt} = \text{rate in} - \text{rate out.}$$
(1)

The rate at which salt enters the tank is the concentration $\frac{1}{4}$ lb / gal times the flow rate r gal / min, or (r/4) lb / min. To find the rate at which salt leaves the tank, we need to multiply the concentration of salt in the tank by the rate of outflow, r gal / min. Since the rates of flow in and out are equal, the volume of water in the tank remains constant at 100 gal, and since the mixture is "well-stirred," the concentration throughout the tank is the same, namely, [Q(t)/100] lb / gal. Therefore, the rate at which salt leaves the tank is [rQ(t)/100] lb / min. Thus the differential equation governing this process is

$$\frac{dQ}{dt} = \frac{r}{4} - \frac{rQ}{100} \cdot Q' + \frac{r}{100} \cdot Q = \frac{r}{4} \quad \text{II(t)} = e^{\frac{1}{100} \cdot t}$$
(2)

The initial condition is

or

$$Q(0) = Q_0$$
. (3)

Upon thinking about the problem physically, we might anticipate that eventually the mixture originally in the tank will be essentially replaced by the mixture flowing in, whose concentration is $\frac{1}{4}$ lb / gal. Consequently, we might expect that ultimately the amount of salt in the tank would be very close to 25 lb. We can also find the limiting amount $Q_L = 25$ by setting dQ / dt equal to zero in Eq. (2) and solving the resulting algebraic equation for Q.

To solve the initial value problem (2), (3) analytically, note that Eq. (2) is both linear and separable. Rewriting it in the standard form for a linear equation, we have

Thus the integrating factor is $e^{rt/100}$ and the general solution is

$$Q(t) = 25 + ce^{-rt/100}, \qquad = e^{100} \qquad \left[\frac{re^{100}}{4}\right] \tag{5}$$

where c is an arbitrary constant. To satisfy the initial condition (3), we must choose $c = Q_0 - 25$. Therefore, the solution of the initial value problem (2), (3) is

$$Q(t) = 25 + (Q_0 - 25)e^{-rt/100}$$

 $O(t) = 25/1 = e^{-tt/100}$

 $Q(t) = 25(1 - e^{-rt/100}) + Q_0e^{-rt/100}$

(continued)

$$Q(t) = 25 + (Q_0 - 25)e^{-rt/100}$$

(6)

ог

$$Q(t) = 25(1 - e^{-rt/100}) + Q_0e^{-rt/100}$$
 (7)

From Eq. (6) or (7), you can see that $Q(t) \to 25$ (1b) as $t \to \infty$, so the limiting value Q_L is 25, confirming our physical intuition. Further, Q(t) approaches the limit more rapidly as r increases. In interpreting the solution (7), note that the second term on the right side is the portion of the original salt that remains at time t, while the first term gives the amount of salt in the tank as a consequence of the flow processes. Plots of the solution for r = 3 and for several values of Q_0 are shown in Figure 2.3.2.

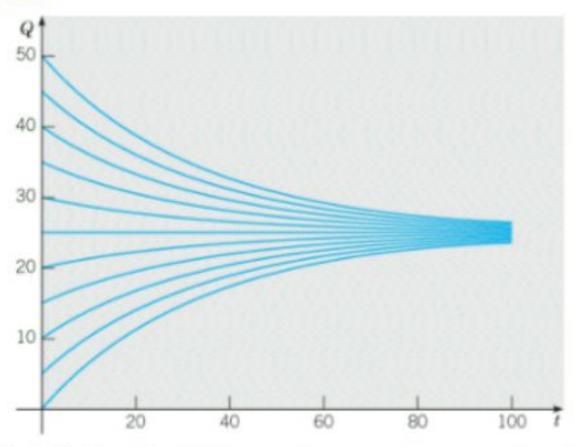


FIGURE 2.3.2 Solutions of the initial value problem (2), (3): dQ / dt = (r / 4) - rQ / 100, $Q(0) = Q_0$ for r = 3 and several values of Q_0 .

Now suppose that r = 3 and $Q_0 = 2Q_L = 50$; then Eq. (6) becomes

$$Q(t) = 25 + 25e^{-0.03t}.$$
(8)

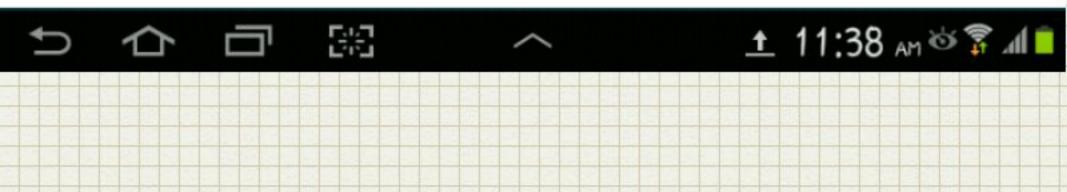
Since 2% of 25 is 0.5, we wish to find the time T at which Q(t) has the value 25.5. Substituting t = T and Q = 25.5 in Eq. (8) and solving for T, we obtain

$$T = (\ln 50) / 0.03 \cong 130.4(\min)$$
 (9)

To determine r so that T = 45, return to Eq. (6), set t = 45, $Q_0 = 50$, Q(t) = 25.5, and solve for r. The result is

$$r = (100/45) \ln 50 \approx 8.69 \text{ gal/min.}$$
 (10)

Since this example is hypothetical, the validity of the model is not in question. If the flow rates are as stated, and if the concentration of salt in the tank is uniform, then the differential equation (1) is an accurate description of the flow process. Although this particular example has no special significance, models of this kind are often used in problems involving a pollutant in a lake, or a drug in an organ of the body, for example, rather than a tank of salt water. In such cases the flow rates may not be easy to determine or may vary with time. Similarly, the concentration may be far from uniform in some cases. Finally, the rates of inflow and outflow may be different, which means that the variation of the amount of liquid in the problem must also be taken into account.



$$\frac{dy}{dx} = x^{4} \Rightarrow \int y dy = \int x^{4} dx \qquad y^{2} - x^{5} \int ||1+3y dy| = \int ||1x^{2}-1| dx|$$

$$y \leftrightarrow \frac{x^{2}}{2} = \frac{x^{5}}{5} + C \qquad \frac{2x^{2}}{2} - \frac{2x^{5}}{3} \qquad \frac{||y+\frac{3}{2}x^{2}| = \frac{11}{3}x^{3} - x + C}{2}$$

$$y'' = \int ||x|^{2} + C \qquad \frac{2x^{2}}{3} - \frac{2x^{5}}{3} \qquad \frac{||y+\frac{3}{2}x^{2}| = \frac{11}{3}x^{3} - x + C}{2}$$

$$y'' = \int ||x|^{2} + C \qquad \frac{2x^{2}}{3} - \frac{2x^{5}}{3} \qquad \frac{||y+\frac{3}{2}x^{2}| = \frac{11}{3}x^{3} - x + C}{2}$$

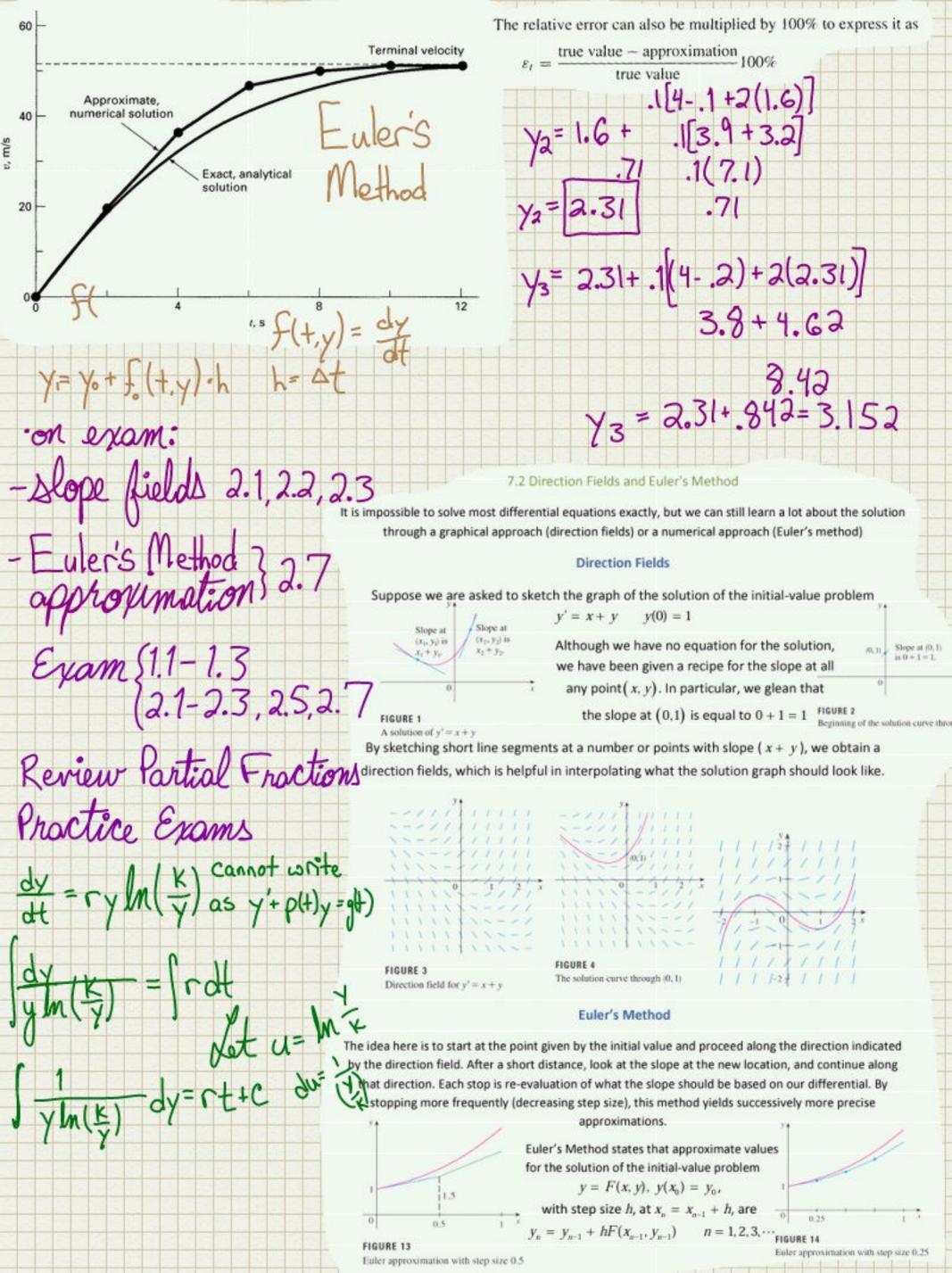
$$\frac{CMm}{R^{2}} \qquad \frac{A^{2}}{R^{2}} = \frac{R^{2}}{R^{2}} = \frac{R^{2}}{R^{2}} = \frac{1}{3}x^{3} - x + C$$

$$\frac{R^{2}}{R^{2}} \qquad \frac{R^{2}}{R^{2}} = \frac{R^{2}}{R^{2}} = \frac{1}{3}x^{3} - x + C$$

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$$\frac{R^{2}$$



$$y'' = f(t,y,y')$$

$$y'' = g(t) - p(t)y' - q(t)y \quad \text{solve for } c, c, \text{ then solve for } c, \text{ and } c_2$$

$$e^{t} \quad ce^{t} \quad t^2e^{t}$$

$$a[r^2e^{t}] + b[re^{t}] + ce^{t} = 0$$

$$e^{t} (ar^2 + br + c) = 0$$

$$ar^2 + br + c = 0 \text{ is called the charactristic equation of the differential equation}$$

$$solve for \ c, \text{ and } c_2$$

$$= -b \pm [b^3 + 0c]^3$$

$$2a$$

$$[r^2 + 5r + 6]e^{rt} = 0$$

$$(r + a)(r + 3) \quad c, e^{2t} + c_2e^{t} = y$$

$$r = -3 \quad c_3 = -3$$

$$y(0) = 3 \quad c_3 + c_4 + c_3 = 3$$

$$y(0) = 3 \quad c_4 + c_4 = 3$$

$$y'(0) = 3 \quad c_4 + c_4 = 3$$

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$$e^{t} (4r^2 \cdot 8r + 3) \quad c_6 = 3 \quad c_4 + c_4 = 3$$

$$4y'' - 8y' + 3y = 0 \quad y(0) = 3$$

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e" = cosut + isinut 16y"-8y'+145y=0 y(0)=-2 y'(0)=1 y"+y'+ 9.25y=0 8 + [64-4(16)(145)] 1/2 (r2+ r+9.25)ert 3 + 96i y+25y=0 y(0)=3 y'(0)=2 32 32 (c2+25)=0 r2+r+9.25=0 -1±[2-4(1)(9.25)]/2 y(t)= c, cosst+c2 sinst $C_1 = 3$ $C_2 = \frac{2}{5}$ -1+51-37 -1±1-36 -1+6i 2 -1+3i,-1-3i -1+3i,-1-3i y'(+) = -15 sin 5t + 5C2cos5t = y'(6)=2 y + dy +y =0 (12+2+1)ert=0 (C+1)(C+1) =0 y=e-rt $y=c_{e}^{-t/2}\cos(3t)+c_{e}^{-t/2}\sin(3t)$ = $e^{-t/2}(c_{e}\cos(3t)+c_{e}\sin(3t))$ y=et y=te-t

y=te-t

y=te-t y(0)=2 y(0)=8 c,=2 g'= y"+4y'+4y=0 eft (12+4+4)=0 e =0 - (r+2)(r+2) r = -2 $y_1 = e^{-2t}y_2 = te^{-2t}$ $c_1 = -2t$ $c_2 = -2t$ $c_3 = 1$ $c_4 = -2t$ $c_4 = -2t$

U= imaginary part By definition. x= real parts. By definition. The Wronskian of the functions of and g 2-4ac <0 ⇒ x = λ± Ui is the determinant f(t) g(t) = f(t)g'(t) - f'(t)g(t). λ>0 → growing exponential envelope f'(t) g'(t) = f(t)g'(t) - f'(t)g(t). λ<0 → decaying exponential envelope = 2± 4 4 = 2± 4± 1 2t 4t - 2t 4t e 4e - 2e e 4e - 2e et = 20 ct 20 → decaying exponential envelope 1=0 → constant oscillation amplitude Look at double angle! t(g'H)-1(glt)=te2t te+te-1(=2+) Loplace transform [= F(s) = [e-st f(t) $\int_{-lpha}^{\infty} f(t) \mathrm{dt} = \lim_{A o \infty} \int_{0}^{A} e^{ct} \mathrm{dt} = \lim_{A o \infty} \frac{1}{c} \left(e^{cA} - 1 \right)$ a mass that weighs & lbs stretches a spring 6 inches. The system is acted on by an external force of 8sin 8t. If the mass is pulled down 3 inches and then released determine the position at all times t. Take g=32 b/s

- ii= ng - ii= n - n=8/32 - 1/4 → F=-KL→ R= 8 = 16 10 → 4 u"+16u=8sin8t → u"+64u=8sin8t 7=±8i y= c, cos(8 t)+ c, sin(8 t) = yp but 8sin 8t - Let yo = Atcas8t + Btsin8t 4Bcos8t+4Acos8t=8sin8t

β= Acos8t-8Atsin8t+Bsin8t+8Btcos8t

β= Acos8t-8Atsin8t+Bsin8t+8Bcos8t+8Bcos8t

μ= C, cos8t+C, sin8t+2tsin8t

1-1-16 Δsin8t+64Δtcos8t+168tcos9t

- CUBLOGAL + (-16 Asin 8+64 Atcos 8+16 Btcos 8+ -64 Btsin 8+) $y=c,\cos 8t+c_2\sin 8t+2t\sin 8t$ $y(0)=3=c_1,c_2=0$ y(0)=0 + 16 $y=3\cos 8t+2t\sin 8t$ 1-64Btsin8t -4Asin8t-16Atcos8t +4B cos8t-16Btsin8t + 16 (At cost + Btsingt)